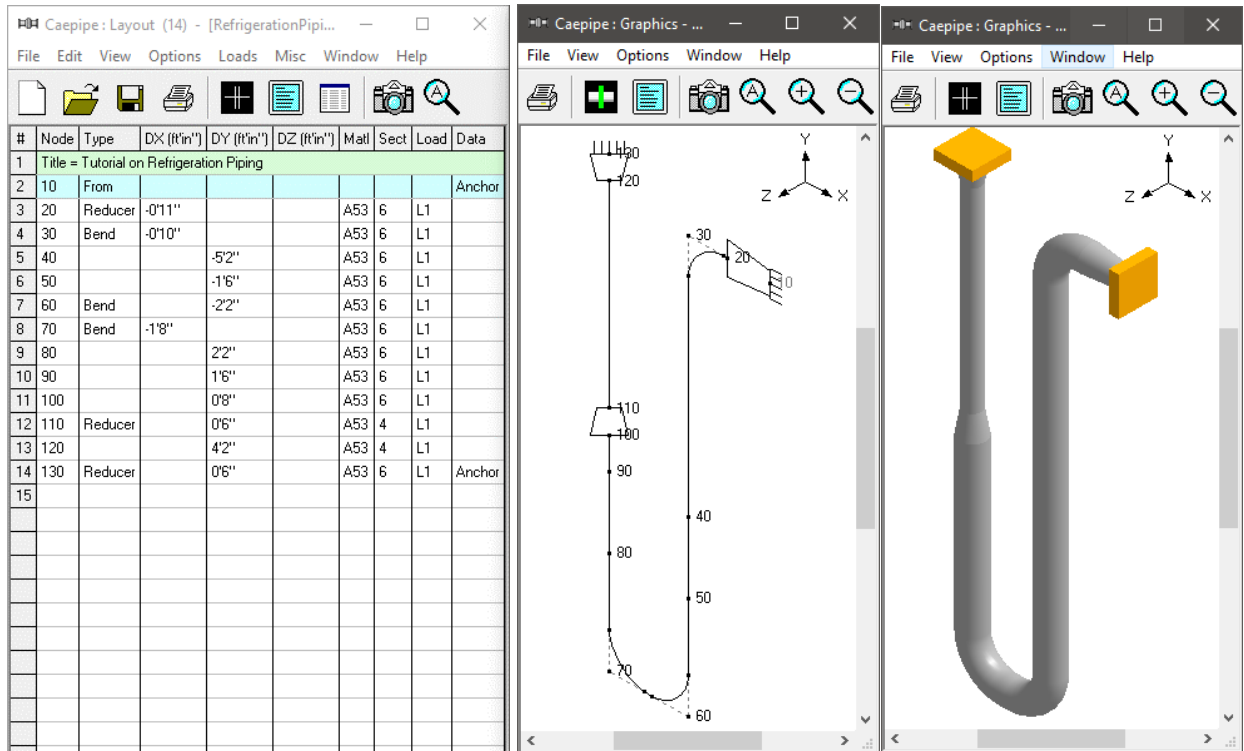


Tutorial on Refrigeration Piping using CAEPIPE

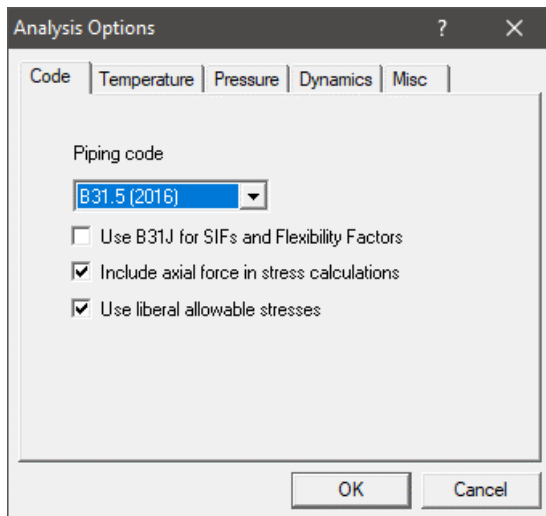
Steps to perform Analysis of Refrigeration Piping with ASME B31.5 Code using CAEPIPE:

The snap shot below shows the sample layout of a refrigeration piping system. The system experiences two (2) different temperatures during its operation (from -50 deg. F to 200 deg. F) with installation temperature as 70 deg. F. Being refrigeration piping, the analysis code is selected as ASME B31.5 for this system.



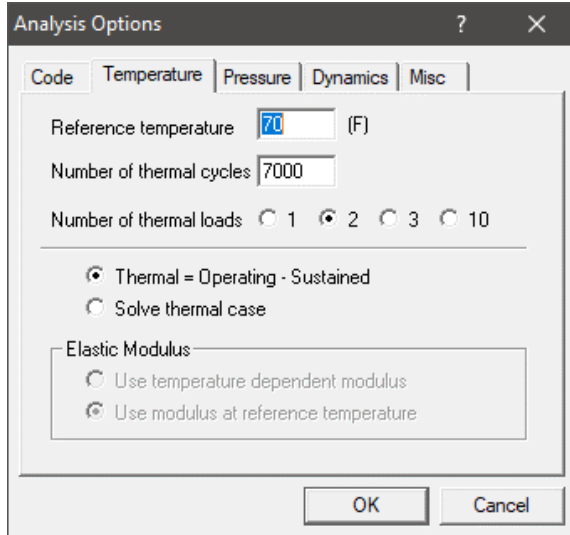
Step 1:

Select the Analysis code as ASME B31.5 through Layout Window > Options > Analysis as shown below.



Step 2:

As the piping layout involves two (2) operating temperatures, “Number of Thermal Loads” needs to be set as “2”. This can be done through Layout Window > Analysis > Temperature as shown below. In addition, the installation temperature (same as “Reference temperature”) can be input as shown below.

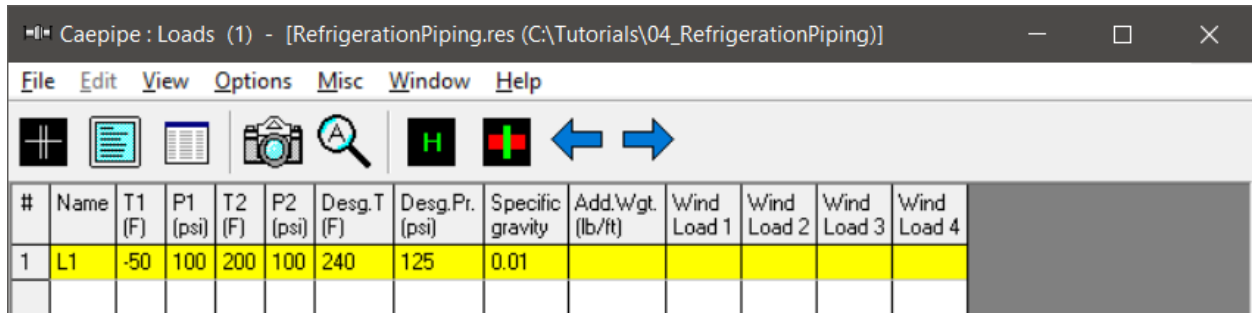


Note:

As per para. 519.4.5(a) of ASME B31.5 (2016), bending and torsional stresses shall be computed using the as-installed modulus of elasticity, i.e., E_c at installation temperature (same as “Reference temperature”). Hence, "Use modulus at reference temperature" is set as "default" and is disabled for user to modify.

Step 3:

Enter the Operating temperatures of the piping layout through “Layout Window > Misc > Loads” as shown below.



Note:

Design Temperature entered will be used to determine the allowable stress for material, which is in turn used to compute the Allowable Pressure as per the piping code selected (B31.5 in this case).

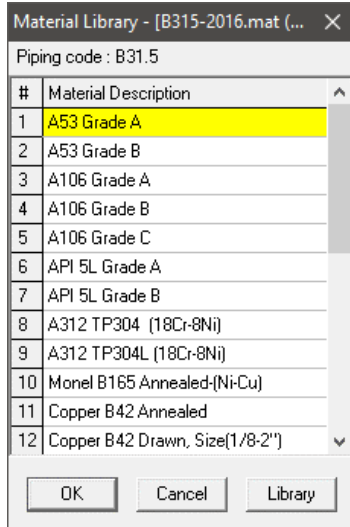
The Allowable Pressure so computed as per the piping code selected is then compared against the Design Pressure entered above and reported in the Code Compliance results.

In addition, starting CAEPIPE Version 10.20, a new load case called “Design (W+PD+TD)” is added. When this load case is selected for Analysis, CAEPIPE will compute and show results for Displacements,

Element Forces & Moments, Support Loads and Support Load Summary. This load cases is NOT included in Stress Calculations, Rotating Equipment Qualifications and Flange Equivalent Pressure Calculations.

Step 4:

Select the material properties corresponding to “A53 Grade A” through “Layout Window > Misc > Materials > File > Library...”.

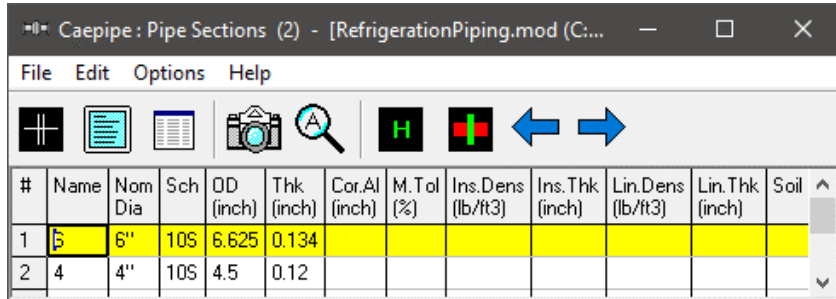


From the dialog box shown, select the Material library as B315-2016 from the folder “Material_Library” available inside the CAEPIPE installation folder. Once selected, highlight the material as shown above and press the button “OK”.

#	Name	Description	Type	Density (lb/in ³)	Nu	Joint factor	#	Temp (F)	E (psi)	Alpha (in/in/F)	Allowable (psi)
1	A53	A53 Grade A	CS	0.283	0.3	1.00	1	-20	29.9E+6	5.89E-6	13700
2							2	70	29.5E+6	6.08E-6	13700
							3	100	29.3E+6	6.14E-6	13700
							4	150	29.1E+6	6.24E-6	13700
							5	200	28.8E+6	6.35E-6	13700
							6	250	28.6E+6	6.62E-6	13700
							7	300	28.3E+6	6.88E-6	13700
							8	350	28.0E+6	6.85E-6	13700
							9	400	27.7E+6	6.82E-6	13700
							10				

Step 5:

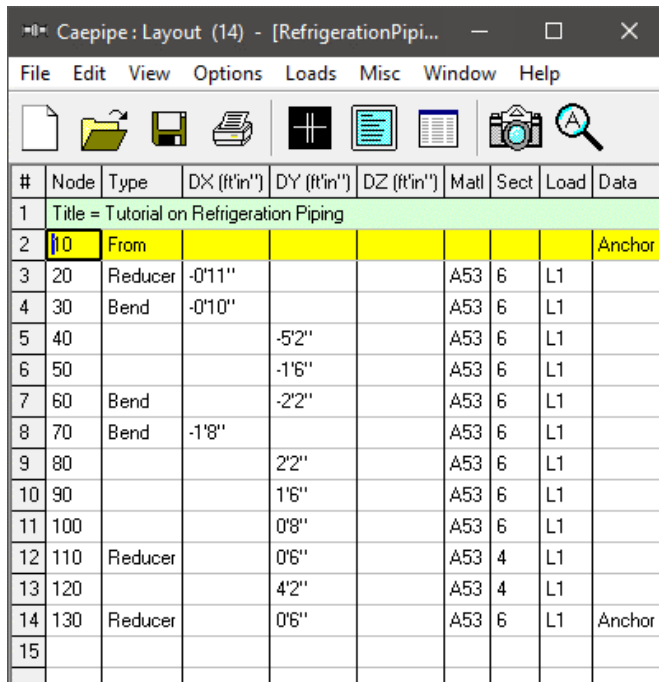
Define the section properties through "Layout Window > Misc > Sections".



#	Name	Nom Dia	Sch	OD (inch)	Thk (inch)	Cor.Al (inch)	M.Tol (%)	Ins.Dens (lb/ft3)	Ins.Thk (inch)	Lin.Dens (lb/ft3)	Lin.Thk (inch)	Soil
1	5	6"	10S	6.625	0.134							
2	4	4"	10S	4.5	0.12							

Step 6:

Generate the piping layout as shown below.

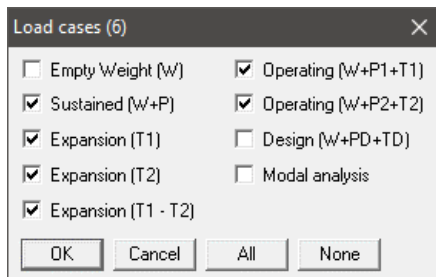


#	Node	Type	DX (ft'in')	DY (ft'in')	DZ (ft'in')	Matl	Sect	Load	Data
1	Title = Tutorial on Refrigeration Piping								
2	10	From							Anchor
3	20	Reducer	-0'11"			A53	6	L1	
4	30	Bend	-0'10"			A53	6	L1	
5	40			-5'2"		A53	6	L1	
6	50			-1'6"		A53	6	L1	
7	60	Bend		-2'2"		A53	6	L1	
8	70	Bend	-1'8"			A53	6	L1	
9	80			2'2"		A53	6	L1	
10	90			1'6"		A53	6	L1	
11	100			0'8"		A53	6	L1	
12	110	Reducer		0'6"		A53	4	L1	
13	120			4'2"		A53	4	L1	
14	130	Reducer		0'6"		A53	6	L1	Anchor
15									

Step 7:

After creating the stress model, turn ON load cases through "Layout Window > Loads > Load cases as shown below.

Expansion (T1) {which is the same as the range (T1 – Tref)}, Expansion (T2) {which is the same as the range (T2 – Tref)}, and Expansion (T1 – T2) [= (T1 – Tref) - (T2 – Tref)].



Load Case	Checked
Empty Weight (W)	<input type="checkbox"/>
Sustained (W+P)	<input checked="" type="checkbox"/>
Expansion (T1)	<input checked="" type="checkbox"/>
Expansion (T2)	<input checked="" type="checkbox"/>
Expansion (T1 - T2)	<input checked="" type="checkbox"/>
Operating (W+P1+T1)	<input checked="" type="checkbox"/>
Operating (W+P2+T2)	<input checked="" type="checkbox"/>
Design (W+PD+TD)	<input type="checkbox"/>
Modal analysis	<input type="checkbox"/>

After analysis, Expansion Stress (SE) value given at any node in Results Window > Sorted stresses and Results Window > Code compliance is the highest thermal stress range at that node among the three thermal ranges (T1 – Tref), (T2 – Tref) and (T1 – T2).

Step 8:

Save the model and perform analysis through Layout window > File > Analyze.

In order to understand the loads and load combinations used for analysis, review the CAEPIPE results file for Sorted Stress, Code Compliance, Displacements, Support Loads (loads acting on the supports by the piping for each load case), Element Forces & Moments (local/global forces and moments on each element for each load case) and Support Load Summary (listing support loads at a particular support for all relevant load cases and load combinations).

As stated above, Sorted Stresses in CAEPIPE lists the maximum of Expansion stresses for all thermal range cases at each node. On the other hand, for Sustained case, it always uses the maximum pressure among the input pressures (P1 and P2 in this case) while computing Sustained Stress at each node.

#	Sustained				Expansion			
	Node	SL (psi)	SH (psi)	SL SH	Node	SE (psi)	SA (psi)	SE SA
1	10	1721	13700	0.13	30A	1116	32700	0.03
2	30A	1550	13700	0.11	10	1025	32529	0.03
3	30B	1494	13700	0.11	70B	780	32883	0.02
4	70B	1367	13700	0.10	30B	758	32756	0.02
5	20	1342	13700	0.10	70A	587	33006	0.02
6	60A	1322	13700	0.10	60B	525	33000	0.02
7	40	1286	13700	0.09	20	323	32908	0.01
8	130	1283	13700	0.09	110	206	33247	0.01
9	80	1276	13700	0.09	120	189	33231	0.01
10	90	1273	13700	0.09	80	179	32974	0.01
11	50	1273	13700	0.09	60A	166	32928	0.01
12	100	1271	13700	0.09	90	128	32977	0.00
13	60B	1250	13700	0.09	100	105	32979	0.00
14	70A	1244	13700	0.09	130	98	32967	0.00
15	120	1019	13700	0.07	40	70	32964	0.00
16	110	1003	13700	0.07	50	19	32977	0.00

Operating Stress for Impact Test can be seen by selecting the option “Show Operating Stress for Impact Test” through Mouse Right click.

Caepipe : B31.5 (2016) Code compliance (Sorted stress...

File Results View Options Window Help

Print, Home, List, Camera, Search, Back, Forward, S, S/A

#	Sustained				Expansion			
	Node	SL (psi)	SH (psi)	SL/SH	Node	SE (psi)	SA (psi)	SE/SA
1	10	1721	13700	0.13	30A	1116	32700	0.03
2	30A	1550	13700	0.11	10	1025	32529	0.03
3	30B	1494	13700	0.11	70B	780	32883	0.02
4	70B	1367	13700	0.10	30B	758	32756	0.02
5	20	1342	13700	0.10	70A	587	33006	0.02
6	60A	1322	13700	0.10	60B	525	33000	0.02
7	40	1286	13700	0.09	20	323	32908	0.01
8	130	1283	13700	0.09	110	206	33247	0.01
9	80	1276	13700	0.09	120	189	33231	0.01
10	90	1273	13700	0.09	80	179	32974	0.01
11	50	1273	13700	0.09	60A	166	32928	0.01
12	100	1271	13700	0.09	90	128	32977	0.00
13	60B	1250	13700	0.09	100	105	32979	0.00
14	70A	1244	13700	0.09	130	98	32967	0.00
15	120	1019	13700	0.07	40	70	32964	0.00
16	110	1003	13700	0.07	50	19	32977	0.00

Context menu: Show Stresses, Show Stress Ratios, Thresholds..., Show Operating Stress for Impact Test, Hide Allowables, Results..., Next Result, Previous Result

Caepipe : B31.5 (2016) Code compliance (Sorted stress...

File Results View Options Window Help

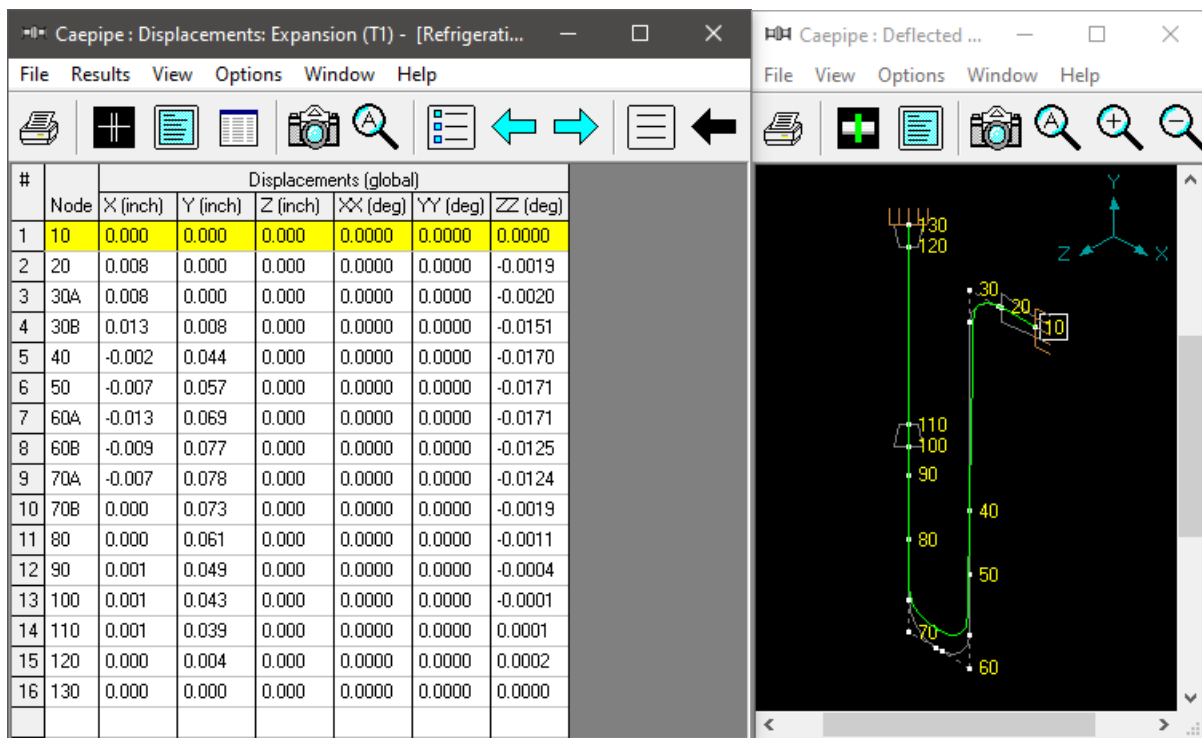
Print, Home, List, Camera, Search, Back, Forward, S, S/A

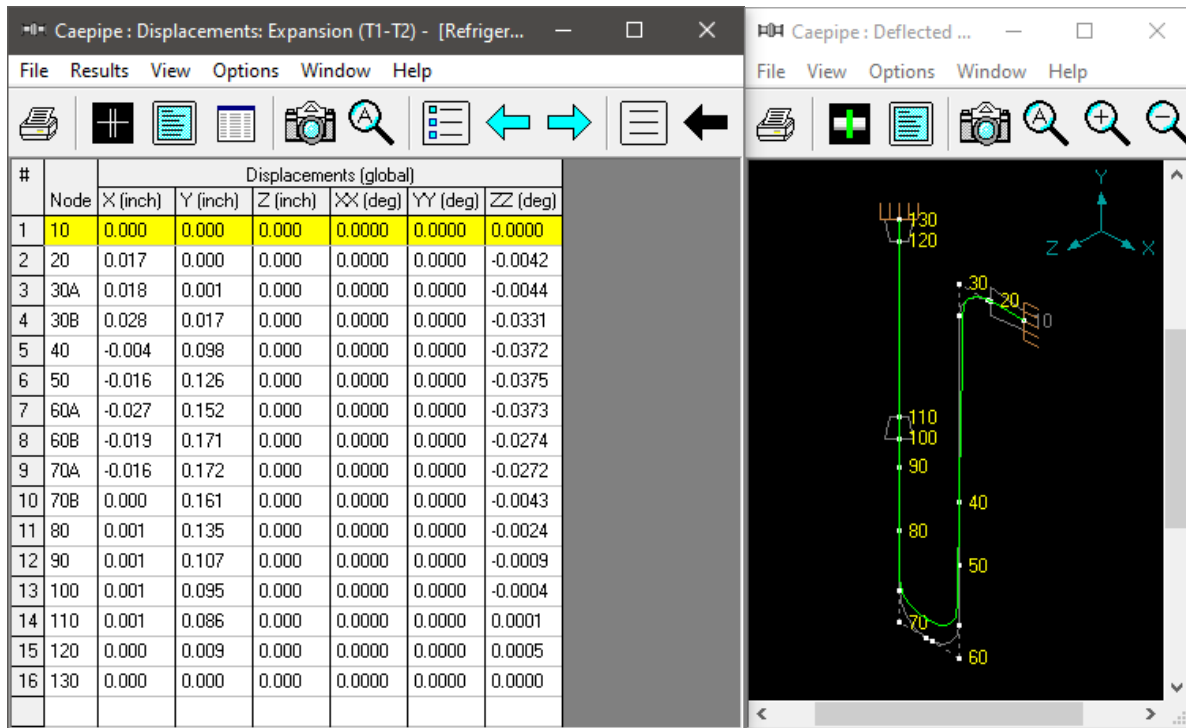
#	Sustained				Expansion				Oper. Stress for Impact Test			
	Node	SL (psi)	SH (psi)	SL/SH	Node	SE (psi)	SA (psi)	SE/SA	Node	Sopr (psi)	Sall (psi)	Sopr/Sall
1	10	1721	13700	0.13	30A	1116	32700	0.03	30B	1828	4795	0.38
2	30A	1550	13700	0.11	10	1025	32529	0.03	70B	1724	4795	0.36
3	30B	1494	13700	0.11	70B	780	32883	0.02	70A	1513	4795	0.32
4	70B	1367	13700	0.10	30B	758	32756	0.02	60B	1464	4795	0.31
5	20	1342	13700	0.10	70A	587	33006	0.02	30A	1434	4795	0.30
6	60A	1322	13700	0.10	60B	525	33000	0.02	80	1358	4795	0.28
7	40	1286	13700	0.09	20	323	32908	0.01	90	1331	4795	0.28
8	130	1283	13700	0.09	110	206	33247	0.01	130	1329	4795	0.28
9	80	1276	13700	0.09	120	189	33231	0.01	100	1319	4795	0.28
10	90	1273	13700	0.09	80	179	32974	0.01	40	1306	4795	0.27
11	50	1273	13700	0.09	60A	166	32928	0.01	20	1279	4795	0.27
12	100	1271	13700	0.09	90	128	32977	0.00	50	1269	4795	0.26
13	60B	1250	13700	0.09	100	105	32979	0.00	10	1260	4795	0.26
14	70A	1244	13700	0.09	130	98	32967	0.00	60A	1245	4795	0.26
15	120	1019	13700	0.07	40	70	32964	0.00	120	1106	4795	0.23
16	110	1003	13700	0.07	50	19	32977	0.00	110	1097	4795	0.23

Similarly, Code Compliance report lists the Stresses element-wise following the same procedure as done for Sorted Stresses.

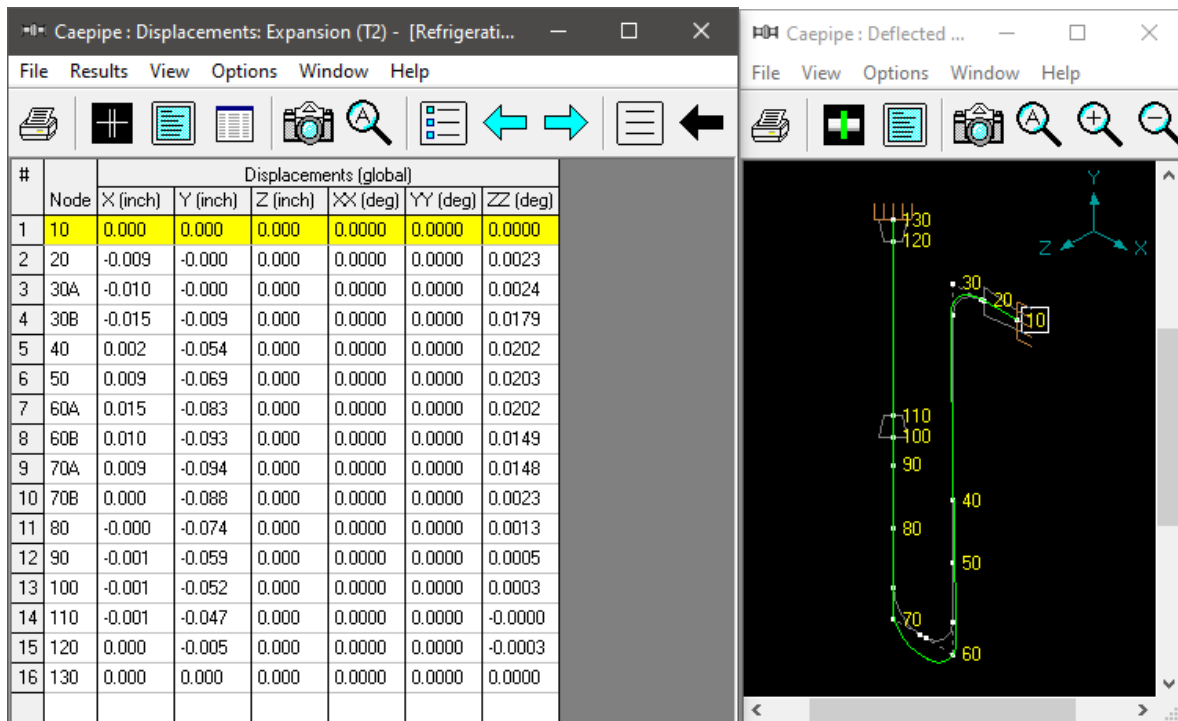
#	Node	Press. Allow. (psi)	Sustained			Expansion		
			SL (psi)	SH (psi)	SL/SH	SE (psi)	SA (psi)	SE/SA
1	10	125	1721	13700	0.13	1025	32529	0.03
	20	563	1342	13700	0.10	323	32908	0.01
2	20	125	1342	13700	0.10	323	32908	0.01
	30A	563	1324	13700	0.10	314	32926	0.01
3	30A	125	1550	13700	0.11	1116	32700	0.03
	30B	563	1494	13700	0.11	758	32756	0.02
4	30B	125	1326	13700	0.10	221	32924	0.01
	40	563	1286	13700	0.09	70	32964	0.00
5	40	125	1286	13700	0.09	70	32964	0.00
	50	563	1273	13700	0.09	19	32977	0.00
6	50	125	1273	13700	0.09	19	32977	0.00
	60A	563	1260	13700	0.09	56	32990	0.00
7	60A	125	1322	13700	0.10	166	32928	0.01
	60B	563	1250	13700	0.09	525	33000	0.02
8	60B	125	1240	13700	0.09	149	33010	0.00
	70A	563	1239	13700	0.09	167	33011	0.01
9	70A	125	1244	13700	0.09	587	33006	0.02
	70B	563	1367	13700	0.10	780	32883	0.02
10	70B	125	1279	13700	0.09	227	32971	0.01
	80	563	1276	13700	0.09	179	32974	0.01

From the Displacement results for Expansion (T1) and Expansion (T1-T2), it is observed that the Displacements are +ve in Global Y direction confirming that the piping is shrinking due to temperature decrease for both expansion cases.





Similarly, from the Displacement results for Expansion (T2), it is observed that the Displacements are -ve in Global Y direction confirming that the piping is expanding downward due to temperature increase.



Element Forces & Moments (local forces and moments on each element for Expansion (T2) load case) are shown below.

Caepipe : Pipe forces in local coordinates: Expansion (T2) - [RefrigerationPiping.res...]

File Results View Options Window Help

#	Node	Axial (lb)	y Shear (lb)	z Shear (lb)	Torsion(ft-lb)		Inplane(ft-lb)		Outplane(ft-lb)		Flex. Factors			SE (psi)
					Moment	SIF	Moment	SIF	Moment	SIF	FFi	FFo	FFt	
1	10	-7	-20	0	0	-81	1.00	0	1.00				556	
	20	-7	-20	0	0	-63	1.00	0	1.00				175	
2	20	-7	-20	0	0	-63		0					175	
	30A	-7	-20	0	0	-61		0					170	
3	30A	-7	20	0	0	61	3.59	0	2.99	13.74	13.74		606	
	30B	20	7	0	0	41	3.59	0	2.99	13.74	13.74		411	
4	30B	20	-7	0	0	-41		0					120	
	40	20	-7	0	0	-11		0					38	
5	40	20	-7	0	0	-11		0					38	
	50	20	-7	0	0	-1		0					11	
6	50	20	-7	0	0	-1		0					11	
	60A	20	-7	0	0	8		0					30	
7	60A	20	-7	0	0	8	3.59	0	2.99	13.74	13.74		90	
	60B	-7	-20	0	0	28	3.59	0	2.99	13.74	13.74		285	
8	60B	-7	-20	0	0	28		0					81	
	70A	-7	-20	0	0	32		0					90	
9	70A	-7	-20	0	0	32	3.59	0	2.99	13.74	13.74		318	
	70B	-20	7	0	0	42	3.59	0	2.99	13.74	13.74		423	
10	70B	-20	-7	0	0	-42		0					123	
	80	-20	-7	0	0	-32		0					97	
11	80	-20	-7	0	0	-32		0					97	
	90	-20	-7	0	0	-22		0					69	

Element Forces & Moments (global forces and moments on each element for Expansion (T2) load case) are shown below.

Caepipe : Pipe forces in global coordinates: Expansion (T2) - [RefrigerationPiping.r...]

File Results View Options Window Help

#	Node	FX (lb)	FY (lb)	FZ (lb)	MX (ft-lb)	MY (ft-lb)	MZ (ft-lb)
1	10	-7	20	0	0	0	-81
	20	7	-20	0	0	0	63
2	20	-7	20	0	0	0	-63
	30A	7	-20	0	0	0	61
3	30A	-7	20	0	0	0	-61
	30B	7	-20	0	0	0	41
4	30B	-7	20	0	0	0	-41
	40	7	-20	0	0	0	11
5	40	-7	20	0	0	0	-11
	50	7	-20	0	0	0	1
6	50	-7	20	0	0	0	-1
	60A	7	-20	0	0	0	-8
7	60A	-7	20	0	0	0	8
	60B	7	-20	0	0	0	-28
8	60B	-7	20	0	0	0	28
	70A	7	-20	0	0	0	-32
9	70A	-7	20	0	0	0	32
	70B	7	-20	0	0	0	-42
10	70B	-7	20	0	0	0	42
	80	7	-20	0	0	0	-32
11	80	-7	20	0	0	0	32
	90	7	-20	0	0	0	-22

Support Loads on all supports by the piping for Operating Load case 1 are shown below.

#	Node	Tag	FX (lb)	FY (lb)	FZ (lb)	MX (ft-lb)	MY (ft-lb)	MZ (ft-lb)
1	10		-8	-70	0	0	0	47
2	130		8	-106	0	0	0	19

Support Load Summary (listing loads on a particular support by the piping) for all relevant load cases and load combinations) is shown below.

Load combination	FX (lb)	FY (lb)	FZ (lb)	MX (ft-lb)	MY (ft-lb)	MZ (ft-lb)
Sustained	-2	-87	0	0	0	115
Operating1	-8	-70	0	0	0	47
Operating2	5	-107	0	0	0	196
Maximum	5	-70	0	0	0	196
Minimum	-8	-107	0	0	0	47
Allowables	0	0	0	0	0	0